



ELEMATIC[®] HOLLOWCORE PLANK

2019 Technical Data Guide for Precast, Prestressed Concrete Hollowcore Plank



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INTRODUCTION

The purpose of this product manual is to provide assistance in selecting and detailing precast concrete hollowcore plank manufactured by Oldcastle Infrastructure.

The load tables presented herein are intended as a guide only. Final design is determined by our engineering department based on information presented in the final plans and specifications. Loading information including SDL, LL, snow drift, and non-uniform concentrated & line loads more than 1.0 kip or 0.100 klf should be stated by the project structural engineer of record (SER). Lateral loading requirements from wind and seismic analysis can be specified in the form of including our standard connection details, or by stating floor diaphragm shear forces in klf on the structural plans. For additional design assistance, please contact us at 518-767-2116 and ask for our engineering dept.

Although care has been taken to provide the most accurate data possible, Oldcastle Infrastructure, Inc. does not assume responsibility for errors and omissions.



MANUFACTURING PROCESS

Elematic[®] is a machine extruded, precast, prestressed hollowcore plank. The planks are manufactured on 600-footlong steel beds in standard widths of 48 inches and thickness of: 8, 10, 12 and 16 inches. High strength prestressing strands are cast into the planks at the spacing and location required for the given span, loading and fire cover conditions. Oldcastle Infrastructure plants are capable of extruding up to 14,000 SF of precast plank every day to meet project schedules. The planks are cut to length for each project using a diamond-blade saw. After the planks are cut, they are removed from the casting beds and placed into storage, and ready for shipment.

All Elematic materials equal or exceed the requirements of applicable ASTM specifications. Our concrete mix is designed to have release strengths of 3,000 psi or 3,500 psi, and a 28-day compressive strength of 5,000 psi. For sustainability, our concrete mix has been fine tuned to use less cement to lower our carbon footprint, but fly ash is not added.

The prestressing strands are uncoated, seven wire, low relaxation with a minimum ultimate strength of 270 ksi.

Our manufacturing capabilities also include: longitudinal and skew cuts to fit any building shape, adding top strands for cantilever designs, cast-in bottom embed plates for welded connections to steel structures, cast-in top plates for curtain wall and relieving angle attachments, column notches, side grout pockets for rebar connections to shear walls, and top slots for field grouting of hollowcores needed for rebar connections and additional shear capacity.

Be sure to discuss your project scope with your Oldcastle sales representative in detail as each project should dictate which details are required for design and constructability.

DELIVERY & INSTALLATION

Oldcastle Elematic[®] Hollowcore Plank plant is located in Selkirk, NY serving the North East region. Our precast hollowcore planks are shipped by truck/trailer to the crane on site (generally less than 500 miles from our plant). Oldcastle's project team will coordinate overall schedule, erection sequence, safety plans, and other project parameters with each customer to ensure on-time delivery.

Our project scope can include installation and grouting by Oldcastle's experienced PCI certified field crews; or FOB delivery only for installation by the general contractor and his/her erector. The erector will install the precast planks in accordance with PCI tolerances which include occasional cutting and trimming of the concrete to adjust for product and field tolerances, and interference with steel connections not shown on contract & shop drawings. Grouting material consists of 1:3 cement-sand grout with a minimum 28-day strength of 2,500 psi placed in all plank joints, and sometimes also at perimeter joints. Higher grout strengths of 4,000 psi is used on CFMF load bearing metal stud and Girder-Slab shallow steel beam structures. Field grout is delivered by ready mix truck and placed by crane, or by grout pump. Pre-packaged non-shrink grout is not used in hollowcore plank grouting.

LOAD TABLE DESIGN CRITERIA

The tables herein list allowable live loads in pounds per square foot (PSF) for uniformly distributed loading. Non-uniform loading conditions resulting from point loads, line loads, openings and cantilevers require special design consideration. The SER should specify the required uniform and special loading on the structural drawings. Oldcastle Infrastructure engineering will perform all engineering analysis and submit PE stamped calculations to the GC/Architect/SER for review and approval prior to fabrication.

Load Table values are calculated in accordance with ACI 318-14 design standard and comply with L/360 deflection limits.

Load tables are based on a plank concrete strength of 5,000 psi. Tables for topped sections are based on a topping strength of 3,500 psi and minimum thickness of 2 inches.

Plank self-weight and 2" concrete composite topping are both included, and do not need to be added to your design loads to compare to these load tables.

See "Notes" section in the load tables for other helpful design tips on using our load tables. It is possible to exceed the values in these load tables by approximately 10% if the area in question is adjacent to side wall or beam support, or shorter spans.

For initial design, the following span to depth ratios (L/D) can be used to determine maximum spans and hollowcore plank thickness:

MAXIMUM SPAN TO DEPTH RATIO						
Residential Loading of 20 SDL + 40 LL	48					
Residential Loading with masonry partitions	35					
Common/Assembly Loading of 10 SDL + 100 LL	42					

PLANK DESIGN CONSIDERATIONS

The following items will affect the selection of appropriate plank sizes and should be carefully reviewed by the Architect/ Engineer (SER = structural engineer of record) while developing the plans and specifications for a project:

LOADING CONDITIONS

- | Specify all uniform loading requirements on structural drawings.
- | Specify snow drift loads per ASCE-7 on the roof plan.
- | The SER should specify plank connection details and/or diaphragm shear forces resulting from wind and seismic lateral analysis; and retained earth if present.
- | Identify line and point loads resulting from masonry partition walls, face brick, posts, mansards, RTUs, mechanical equipment, etc.
- | In general, the plank floor system can be designed for MEP openings and small skylights less than 4'-0" wide.
- | Larger openings such as elevator shafts, stair shafts, and MEP shafts larger than 4'-0" wide will require additional structural support for the precast planks.

TOPPING

- Specify whether or not concrete topping is to be composite. Composite action requires the topping to be bonded to the top surface of the plank. Oldcastle's standard is to provide a longitudinal machine drag rake finish on the top of the precast planks to provide an intentionally roughened finish for improved bonding with the composite topping.
- "Topped" load tables are calculated with a maximum horizontal shear stress of 80 psi between the top of the precast plank and the bottom of the topping.
- | Topping separated by a vapor barrier or insulation is non-composite and must be considered a superimposed dead load.
- | Large cambers resulting from heavy loads will affect the quantity of topping, assuming a level floor is required. 1-1/2" of composite topping at mid span is minimal, and additional thickness at the ends of the plank may be required to maintain level floor elevations.
- Bonding agent is typically not required on Oldcastle longitudinally raked top finish, unless specified by the SER and/or project specifications.

CAMBER

- Camber is inherent in all prestressed products. It is the result of the eccentric prestress force required to resist design loads, and cannot be designed in, out, or to an exact number. The amount of camber will depend upon the design loads, span and thickness of plank. Planks stored in the yard for more than 4 weeks, usually due to construction schedule changes, will experience more camber growth.
- | Adjacent plank of dissimilar length or dissimilar strand pattern will have inherent camber differences.
- | Joints at plank span change in direction is a common location with differential camber. Building layouts should minimize plank change in direction occurences.
- | Camber can be approximated as 0.3% of the span and must be taken into account when specifying concrete topping thickness. For example, if 2-1/2" concrete topping thickness is specified, a minimum topping thickness of 1-1/2" is still achieved with a maximum plank camber of 1" at mid-span.

The approximate short term camber loss from 30 psf live load is 1/4". This value can be used as a guide for curtain wall connection design to the perimeter edge of the precast plank. The precast plank will revert back to full camber once the live load is gone.

| The approximate long term camber loss from material shrinkage & creep is 1/8" in 5 years and 1/4" in 20 years.

OPENINGS

- | Openings can be reviewed by Oldcastle engineering for the architect/engineer of record during design development, if requested.
- After a project is awarded, Oldcastle engineering will review all openings for structural design during the shop drawing submittal process.
- | Electrical and plumbing openings are typically located and core drilled on site by the MEP sub trade. Larger HVAC openings are located on site by the mechanical sub and saw cut on site by the GC's precast erector or Oldcastle, depending on the executed project scope.
- | Core drilled openings 6" dia. or smaller in isolated situations (ie. not multiple openings next to one another) can be done anywhere, except at a free plank edge. The side of a plank that is not grouted next to another plank or side bearing over a support wall is a free plank edge.
- | Typically, an allowance of approximately 15% of the strands in any plank can be cut without falling below the design load requirements.
- If several openings are in the same vicinity, it is best to have them in a line and parallel to the plank span. This will result in the lost of only one strand, because the same strand is being cut in several locations rather than different strands being cut.
- The planks will support more openings cut near either support ends than in the middle 3rd of the span. This is because the precast planks can be reinforced to restore shear capacity, but not for flexural bending capacity.
- For HVAC duct openings between 20" and 48" wide in size, it is better to locate at a plank joint so that two adjacent planks get cut ½ the width of the opening rather than cutting the entire opening in one plank.
- In areas where the planks are supporting additional heavy loads such as masonry partition walls, the amount of openings than can be cut will be greatly diminished as there is not enough capacity that can be manufactured into the precast planks.
- Generally, the electrical and sprinkler trades can be accommodated since they have small openings. Hand drilled openings will not be able to cut through the strands. The trades will have to make sure that they drill through the core locations.
- We, the plank manufacturer have to approve all openings prior to cutting except those smaller openings less than 6" dia. Typically this is done by forwarding us a copy of the mechanical and plumbing subcontractor's layout drawings. Note that we may not be able to approve excessive opening requirements unless additional framing support is provided.
- On more complex projects with more openings, Oldcastle can provide a full scale template that can be placed on the hollow-core plank deck, using the grout joints to position the template. The template will help identify the location of every hollow cell and strand in any plank. This will allow the MEP trades to make small changes in the final location of cored openings to avoid cutting some of the strands.

FIRE RATING

Fire rating specifications are as important as all other design parameters. Plank rating requirements are determined by the Architect or Structural Engineer of Record (SER), who is also responsible for establishing the fire rating criteria for the total project.

Four methods generally used for determining precast hollow core plank fire-resistant ratings are:

- | 2015 ICC International Building Code
- | Underwriters Laboratories Fire Resistance Ratings
- | NYC OTCR approved product & manufacturer certification (New York City only)
- | Rational analysis as defined by PCI MNL 124, "Design for Fire Resistance of Precast Concrete"

INTERNATIONAL BUILDING CODE "IBC" FIRE RATINGS

The ICC-IBC code prescribes fire ratings to any precast hollowcore plank section. Since 2000, the ICC-IBC code has replaced the BOCA, SBC and UBC model codes in all 50 states. The two criteria that are measured to determine the fire rating are:

- | Equivalent concrete thickness 4.6" is required for 2 hrs
- | Bottom strand cover 34" cover is required for 2 hrs (restrained condition)

UNDERWRITERS LABORATORIES FIRE RESISTANCE RATINGS

Prior to codes including prescriptive fire-endurance rating methods, fire tests provided the primary source of ratings classifications. While some plank sections were fire tested, others can be evaluated by UL from similar existing UL ratings. The table below lists the UL ratings available with Elematic plank. Note that these ratings are dependent upon whether or not the ends of the planks are restrained. Determination of the restraint must be made by the Architect or the Structural Engineer of Record (SER), as it is primarily a function of the support structure.

	RATINO	G (HOUR)	PLANK THICKNESS	TOPPING THICKNESS (INCH)	
UL NUMBER	RESTRAINED	UNRESTRAINED	(INCH)		
J994	11/2	11/2	8, 10, 12	0	
J994	2	11/2	8, 10, 12	1 ^{1/2} Gypcrete	
J994	3 1 ^{1/2}		8, 10, 12	2 ^{1/8} Topping	
J994	4	11/2	8, 10, 12	3 ^{3/8} Topping	
J995	2	2	8, 10, 12	0	
J995	3	2	8, 10, 12	1 ^{1/2} Topping	
J995	4	2	8, 10, 12	2 ^{5/8} Topping	

NEW YORK CITY OTCR PRODUCT APPROVAL

For projects within New York City, the NYC Dept. of Building requires the precast hollowcore manufacturing plant to be pre-approved by the Office of Technical Certification & Research (OTCR). Historically, this certification was known as the MEA certification (Material & Equipment Acceptance) prior to the 2008 NYC Building Code. Oldcastle Infrastructure has been a NYC approved precast hollowcore plank manufacturer since the early 1970s.

FIRE RATINGS BY RATIONAL ANALYSIS

PCI MNL 124 defines the "rational analysis" method for determining the fire resistance rating of precast/ prestressed members. It is useful to use when a fire resistance rating cannot be obtained by any of the three previous methods. Actual practice has shown that this method is very conservative and that the span of the hollowcore plank will have to be reduced (approx. 10% to 20%) to achieve the same fire resistance rating from both IBC and UL.

In using this method, the reduced strength of the prestressed strands at elevated temperatures is determined and the resulting moment capacities are compared to that required for service loads. Strand temperatures are based on the amount of concrete cover and the standard fire exposure as defined by the time-temperature relationship specified in ASTM E119. Fire ratings will also be improved if the plank assembly is restrained against thermal expansion. It should be noted that the only universally accepted definition of full restraint is an interior bay of a multi-bay building.

THERMAL "R" VALUES

Concrete is a dense material, and as a result, is not a good insulating material. On occasion, a designer who needs the thermal "R" value of precast concrete hollowcore planks, can reference the table below.

Although there is some improvement for filling the plank hollowcores with foam insulation, the losses from thermal bridging of the concrete webs greatly reduces the effectiveness of the added insulation. There is also a cost premium and longer lead time associated with adding foam insulation. A much more economical design option is to specify 1'-3" of batt insulation (widely available in 15" rolls) installed into the cores at areas of high potential heat loss, in the field by the general contractor.

THERMAL "R" VALUES	
8" Elematic®	1.34
8" Elematic $^{\scriptscriptstyle (\! 8\!)}$ with foam insulation in cores	3.14
H8" Heavy Elematic®	1.43
H8" Heavy Elematic® with foam insulation in cores	2.72
H10" Heavy Elematic®	1.73
H10" Heavy Elematic $^{\ensuremath{\circledast}}$ with foam insulation in cores	4.05
12" Elematic®	1.91
12" Elematic® with foam insulation in cores	5.01
16" Elematic®	2.28
16" Elematic® with foam insulation in cores	7.48
2" concrete topping	+0.15
3" concrete topping	+0.23
2" lightweight concrete roof topping (110 pcf)	+0.35
4" lightweight concrete roof topping (110 pcf)	+0.70
6" lightweight concrete roof topping (110 pcf)	+1.05

SOUND RATINGS

The following tables contain values for the Sound Transmission Class (STC) and the Impact Insulations Class (IIC) of various floor systems utilizing Elematic[®] Hollowcore Plank precast hollowcore plank.

SOUND TRANSMISSION CLASS (STC)

The values for the Sound Transmission Class were determined by testing in accordance with ASTM E90. The STC is a measure (in decibels) of the ease at which air-borne sound is transmitted through a floor system. The density and mass of precast concrete planks is ideal for achieving larger STC values, which indicate greater sound insulation.

IMPACT INSULATION CLASS (IIC)

The values for the Impact Insulation Class (IIC) were determined by tests which were in accordance with ASTM ES492. Impact Insulation Class is the resistance to impact noise transmission and is mostly influenced by the finish material applied on top of the precast planks. A soft material such as carpeting will achieve the best IIC ratings. As with STC, the higher IIC values are more desirable. Note that IIC testing is typically done by the finish material manufacturer on 6" solid concrete slabs. These test values can be used on other slab thickness and precast hollowcore planks since the effect of the mass of the underlying slab is negligible for impact noise absorption.

SOUND TRANSMISSION CLASS	i (STC)
8" Elematic®	51
8" Elematic® + 2" Topping	54
H8" Heavy Elematic®	51
H8" Heavy Elematic® + 2" Topping	55
H10" Heavy Elematic®	53
H10" Heavy Elematic® + 2" Topping	56
12" Elematic®	54
12" Elematic® + 2" Topping	57
16" Elematic®	56
16" Elematic [®] + 2" Topping	59

IMPACT INSULATION CLASS (IIC)							
TYPES OF FLOOR SYSTEMS	RATING						
8" Hollowcore Plank	28						
8" Hollowcore Plank + ^{1/2} " wood block flooring adhered directly	47						
8" Hollowcore Plank + VTC, (ex. Armstrong)	47-56						
8" Hollowcore Plank + quarry tile w/reinforced mortar bed with 0.4" nylon & carbon black spinneret matting	54						
8" Hollowcore Plank + pad & carpet	73						
Add Acoustical Ceiling	+6						

SUSTAINABILITY

It is recognized that the production of cement contributes to overall greenhouse gas emissions. In 2013, a joint LCA study conducted by the Precast Concrete Institute (PCI), Canadian Prestressed Concrete Institute (CPCI), and the National Precast Concrete Association (NPCA) confirmed this and also gave our industry a benchmark for future improvements. The following sustainable practices are already in place to manufacture, deliver and install our Elematic® hollowcore planks:

- | Use the lowest cement content in manufacturing while still achieving consistent concrete strengths.
- Although fly ash can be added to divert the fly ash waste from landfills, we cannot replace any more cement from our optimized concrete mix.
- Advance machine extrusion technology casts Elematic[®] hollowcore planks with 44%-52% less concrete compared to the equivalent thickness solid concrete slab.
- Proven prestressing technology since the 1960s with ASTM A416 steel strands with 270 ksi yield strength (4.5X stronger than conventional rebar) increases our maximum span by approx. 75% more than continuous design CIP solid concrete slabs of the same thickness which results in less framing elements such as columns, beams, and bearing walls.
- ASTM A615 rebar is ordered to length and cut from continuous coils by our steel fabricator to minimize waste.Steel casting beds provide the most consistent smooth bottom finish without any other additional forming waste (ie. no wood).
- | Both radiant heating in our casting beds and natural curing are used depending on the season to achieve proper curing with the lowest energy use. Steam curing is not used.
- All our concrete constituent materials including cement, limestone aggregates, and sand; are extracted from nearby sources well within the 500 miles LEED criteria.
- All water is pumped from on site wells, reducing the demand on the local municipal water supply.
- Waste precast hollowcore plank in our yard is crushed and separated in our yard. The crushed concrete is used for clean fill material by local road contractors and land owners. All scrap steel is delivered to recycling centers.
- | On the job site, up to 10,000 sf of Elematic[®] Hollowcore Planks can be installed in a single day which reduces the overall duration of the construction process. Larger projects may have two cranes installing precast to further reduce the overall construction duration.
- | The offsite pre-fabrication of precast concrete structural elements greatly reduces on-site construction activities and associated traffic, waste, noise, and safety hazards.

Oldcastle Infrastructure continues to search for more future sustainable practices.

SPECIFICATIONS FOR PRECAST, PRESTRESSED HOLLOWCORE PLANK - SECTION 034100

1. GENERAL

1.01 DESCRIPTION

- A. Work Included:
 - 1. These specifications cover manufacture, transportation and erection of precast, prestressed, concrete, hollowcore plank, including grouting of joints between adjacent units.
- B. Related Work Specified Elsewhere:
 - 2. Cast-in-Place Concrete: Section_____
 - 3. Architectural Precast Concrete: Section_____
 - 4. Precast Structural Concrete: Section _____
 - 5. Underlayments (Floor and/or Roof Leveling): Section_____
 - 6. Caulking and Sealants: Section _____
 - 7. Small Holes for Mechanical/Plumbing: Section _____
 - 8. Cast-in-Place Embedments: Section_____
 - 9. Steel Bearing Lintels: Section _____
 - 10. Insulation in Plank Cores: Section _____

1.02 QUALITY ASSURANCE

A. Manufacturer Qualifications: The precast concrete manufacturing plant shall be certified by the Prestressed Concrete Institute (PCI) Plant Certification Program prior to the start of production. Manufacturer shall be certified in category C2.

The manufacturer shall retain a registered structural engineer to certify that manufacturing is in accordance with design requirements; or

The manufacturer shall, at his expense, meet the following requirements:

- 1. The basis of inspection shall be the Prestressed Concrete Institute's "Manual for Quality Control for Plants and Production of Precast and Prestressed Concrete Products", MNL-116, and the criteria for acceptance shall be the same as the Plant Certification Program.
- B. Erector Qualifications: PCI Qualified and regularly engaged for at least 5 years in the erection of precast structural concrete similar to the requirements of this project. Retain a registered structural engineer to certify that erection is in accordance with design requirements.
- C. Welder Qualifications: In accordance with AWS D1.1.
- D. Testing: In general compliance with applicable provisions of Prestressed Concrete Institute MNL-116, "Manual for Quality Control for Plants and Production of Precast Prestressed Concrete Products".
- E. Requirements of Regulatory Agencies: All local codes plus the following specifications, standards and codes are a part of these specifications:
 - 1. ACI 318 Building Code Requirements for Reinforced Concrete;
 - 2. AWS D1.1 Structural Welding Code-Steel;
 - 3. AWS D1.4 Structural Welding Code-Reinforcing Steel;
 - 4. ASTM Specifications As referred to in Part 2-Products, of this Specification.

1.03 SUBMITTALS AND DESIGN

- A. Shop Drawings:
 - 5. Erection Drawings
 - a. Plans locating and defining all hollowcore planks furnished by the manufacturer, with all major openings shown.
 - b. Sections and details showing connections, weld plates, edge conditions and support conditions of the hollowcore plank units.
 - c. All dead, live and other applicable loads used in the design.
 - d. Fire rating.
- B. Approvals:
 - 1. Submit _____ copies of erection drawings for approval prior to fabrication. Fabrication not to proceed prior to receipt of approved drawings.
 - 2. Alternatively, submit electronic files (ie. PDF) either by email to the CM/GC, or by uploading to internet based project submittal sites.
- C. Product Design Criteria:
 - 1. Loadings for design
 - a. Initial handling and erection stresses.
 - b. All dead and live loads as specified on the contract documents.
 - c. All other loads specified for hollowcore plank where applicable.
 - 2. Fire rating shall be ____ hour(s).
 - 3. Design steel plank support headers when such headers are determined necessary by the manufacturer's engineer.
 - 4. Design calculations shall be performed by an engineer, registered in the state that the project is located in, and experienced in precast prestressed concrete design. Design calculations to be submitted for approval upon request.
 - 5. Design shall be in accordance with ACI 318 building code requirements for structural concrete and applicable codes.
- D. Permissible Design Deviations:
 - 1. Design deviations will be permitted only after the Architect/Engineer's written approval of the manufacturer's proposed design supported by complete design calculations and drawings.
 - 2. Design deviations shall provide an installation equivalent to the basic intent without incurring additional cost to the owner.
- E. Test Reports: Test reports on concrete and other materials shall be submitted upon request.

2. PRODUCTS

2.01 MATERIALS

- A. Portland Cement:
 - 1. ASTM C150 Type I or III.
- B. Admixtures:
 - 1. Water Reducing, Retarding, Accelerating, High-Range Water Reducing Admixtures: ASTM C494

- C. Aggregates:
 - 1. ASTM C33 or C330
- D. Water: Potable or free from foreign materials in amounts harmful to concrete and embedded steel.
- E. Reinforcing Steel:
 - 1. Bars:

Deformed Billet Steel: ASTM A615 Deformed Rail Steel: ASTM A616 Deformed Axle Steel: ASTM A617 Deformed Low Alloy Steel: ASTM A706

- 2. Wire: Cold Drawn Steel: ASTM A82.
- F. Prestressing Strand:
 - 1. Uncoated, 7-Wire, Low Lax strand: ASTM A416 (including supplement) Grade 250K or 270K.
- G. Welded Studs: In accordance with AWS D1.1.
- H. Structural Steel Plates and Shapes: ASTM A36.
- I. Grout:
 - 2. Cement grout: Grout shall be a mixture of not less than one part portland cement to three parts fine sand, and the consistency shall be such that joints can be completely filled but without seepage over adjacent surfaces. The grout shall achieve a minimum 28-day compressive strength of 2,500 psi. Any grout that seeps from the joint shall be completely removed before it hardens.
- J. Bearings Strips:
 - 1. Plastic: Multi-monomer plastic strips shall be non-leaching and support construction loads with no visible overall expansion.

2.02 CONCRETE MIXES

- A. 28-day compressive strength: Minimum of 5,000 psi
- B. Release strength: Minimum of 3,000 psi
- C. Use of calcium chloride or admixtures containing chlorides is not permitted.

2.03 MANUFACTURE

- A. Hollowcore plank shall be machine cast in 48-inch widths under the trade name Elematic[®] as manufactured by Oldcastle Infrastructure.
- B. Manufacturing procedures and tolerances shall be in general compliance with PCI MNL 116.
- C. Openings: Manufacturer shall engineer the planks for rectangular openings 10" or larger on all sides and as clearly shown on the architectural and structural drawings. They shall be located by the trade requiring them and then field cut. Round and small openings (less than 10") shall by drilled, cored drilled or saw cut by the respective trades after grouting. Openings requiring cutting of prestressing strand shall be approved by the precast plank manufacturer before drilling or cutting.
- D. Finishes: Bottom surface shall be flat and uniform as resulting from an extrusion process, without major chips, spalls and imperfections. Top surface shall be machine troweled.
- E. Patching: Will be acceptable providing the structural adequacy of the hollow core unit is not impaired.

3. EXECUTION

3.01 PRODUCT DELIVERY, STORAGE AND HANDLING

- A. Delivery and Handling:
 - Hollowcore plank shall be lifted and supported during manufacturing, stockpiling, transporting and erection operations only at the lifting or supporting points designated by the manufacturer. The erector should place lift cables or straps at the two dunnage locations on the delivery trailer, for each hollowcore plank.
 - 2. Transportation, site handling and erection shall be performed by qualified personnel with acceptable equipment and methods.
- B. Storage:
 - 1. Store all units off ground on firm, level surfaces with dunnage placed at bearing points.
 - 2. Place stored units so that identification marks are discernible.
 - 3. Separate stacked units by dunnage across full width of each plank.

3.02 ERECTION

- A. Site Access: Erection access suitable for cranes and trucks to move unassisted from public roads to all crane working areas as required by erector, or otherwise indicated herein, will be provided and maintained by the general contractor. Obstructing wires shall be shielded or removed and, when applicable, snow removal and winter heat will be provided by the general contractor.
- B. Preparation: The general contractor shall be responsible for:
 - 1. Providing true, level, bearing surfaces on all field-placed bearing walls and other field placed supporting members. Masonry wall bearing surfaces shall be bond beams with properly filled and cured concrete.
 - 2. All pipes, stacks, conduits and other such items shall be stubbed off at a level lower than the bearing plane until after the planks are set. Masonry, concrete or steel shall not be installed above plankbearing surface until after the plank is in place.
- C. Installation: Installation of hollowcore slab units shall be performed by the PCI certified erector. Members shall be lifted with slings at points determined by the manufacturer. Bearing strips shall be set where required. Grout keys shall be filled. Openings shall be field cut only after grout has cured, unless authorized by the manufacturer's engineer.
- D. Alignment: Members shall be properly aligned. Variations between adjacent members shall be reasonably leveled out by jacking, bolting or any other feasible method as recommended by the manufacturer and the PCI Erector's Manual (MNL-127-99).
- E. Weep Holes: Drilling 1/2"Ø to 3/4"Ø weep holes, typically 1'-0" from the ends of the planks beyond where grouting has flowed into the hollow-cores as required; to allow trapped water to drain out. Sources of trapped water can include rain, snow melt, wet coring and saw cutting, and deck cleaning for topping placement preparation. The general contractor should also look for signs of more trapped water at the lower floors of installed hollowcore plank as trapped water tend to migrate down to the lower floors (darker stained bottom finish and sometimes water droplets are visible). MEP and hung ceiling trades installing their work to the ceiling should also be prepared for unexpected water draining out as they drill into the bottom of the hollow-core plank. It is not recommended to leave trapped water in the plank as that can cause freeze spalls in winter conditions, mold, and damage to paint and other finish materials. Patching of weep holes in exposed ceiling areas is required after building is water tight and rooms are heated to a minimum of 40 degrees to provide for proper bonding of patching material."

3.03 FIELD WELDING

A. Field welding is to be done by qualified welders using equipment and materials compatible to the base material.

3.04 ATTACHMENTS AND SMALL HOLES

A. Subject to approval of the Architect/Engineer, hollowcore plank units may be drilled or "shot" provided no contact is made with the prestressing steel. Round holes and those less than 8 inches on any side shall be drilled or cut by the respective trades. Should spalling occur, it shall be repaired by the trade doing the drilling, shooting or cutting.

3.05 CLEAN UP

A. Remove rubbish and debris resulting from hollowcore plank work from premises upon completion.

3.06 SAFETY

A. The general contractor will provide and maintain all safety barricades, rebar caps and opening covers required for plank in accordance with current industry safety standards.

PRODUCTION & ERECTION TOLERANCES

PRODUCT TOLERANCES: HOLLOWCORE SLABS

b		
	=	Width $+1/4$ in
С	=	Denth $+1/4$ in
d t	=	Ton flange thickness
l		Ton flange area defined by the actual measured values of average d, x b shall not be
		loss than 95% of the nominal area calculated by d _ nominal v h nominal
d.	=	
ч ()	Bottom flange thickness
		Bottom flange area defined by the actual measured values of average d b x b shall not
		be less than 85% of the nominal area calculated by d $_{ m b}$ nominal x b nominal.
е	-	Web thickness
		The total cumulative web thickness defined by the actual measured value Σ e shall not
		be less than 85% of the nominal cumulative width calculated by Σ e nominal.
f	=	Blockout location
g	=	Flange angle
h	=	Variation from specified end squareness or skew $\pm^{1}/_{2}$ in.
i	=	Sweep (variation from straight line parallel to centerline of member) $\dots \pm \frac{1}{8}$ in.
j	=	Center of gravity of strand group
		The CG of the strand group relative to the top of the plank shall be within $+1/4$ in of the
		nominal strand drown CG. The position of any individual strand shall be with $\frac{1}{2}$ in of
		nominal vertical position and $\frac{1}{3}$ in of nominal horizontal position and shall have a
		minimum cover of $+3/4$ in
k	=	Desition of plates ± 2 in
I	=	Tinning and Auchnoos of plates
m	=	Local emosthese 11/ in in 10 ft
		Local smoothes \mathbf{T} /4 III. III 10 II.
		(does not apply to top deck surface left rough to receive a topping or to visually con-
C	lon	Cealed Suffaces) Is weight: Excess concrete material in the plank internal features is within telerance as
E E	'Idll	is weight, excess concrete material in the plank internal reactives is within tolerance as
10	ung	as the measured weight of the head associate solution to exceed 110% of the norminal
p n	ומטנ	isned unit weight used in the load capacity calculation.
	_	Applications requiring class control of differential compar between adjacent members
	=	Applications requiring close control of differential camber between adjacent members
	=	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine
	=	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances.
EF	= RE	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE
EF FL	= ?E	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS
EF FL a	= RE .0(Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE OR & ROOF MEMBERS Plan location from building grid datum
EF FL a	= RE .0(=	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE OR & ROOF MEMBERS Plan location from building grid datum
EF FL a a b	= .0(= 1 = =	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE OR & ROOF MEMBERS Plan location from building grid datum
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a a b	= RE .0(= =	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum. ± 1 in. Plan location from centerline of steel ¹ ± 1 in. Top elevation from nonminal elevation at member ends $\pm^{3}/_{4}$ in Covered with topping $\pm^{1}/_{4}$ in. Untopped floor $\pm^{3}/_{4}$ in.
E F a a 1 b	= RE .0(= = =	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum
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e E F L a a 1 b c d	= .0(= = = =	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum
e e	= .0(= = =	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE OR & ROOF MEMBERS Plan location from building grid datum. ± 1 in. Plan location from centerline of steel ¹ ± 1 in. Top elevation from nonminal elevation at member ends $\pm 3/4$ in Covered with topping $\pm 3/4$ in. Untopped floor $\pm 3/4$ in. Maximum jog in alighment of matching edge $\pm 3/4$ in. (both topped and untopped construction) ± 1 in. Joint width; 0 to 40 ft. member length $\pm 1/2$ in. 41 to 60 ft. member length $\pm 3/4$ in. Differential top elevation as erected. $3/4$ in. Covered with topping $3/4$ in.
e f		Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum. ± 1 in. Plan location from centerline of steel ¹ ± 1 in. Top elevation from nonminal elevation at member ends $\pm 3/4$ in Covered with topping $\pm 3/4$ in. Untopped floor $\pm 3/4$ in. Maximum jog in alighment of matching edge $\pm 3/4$ in. (both topped and untopped construction) ± 1 in. Jifferential top elevation as erected. $\pm 3/4$ in. Covered with topping $\pm 3/4$ in. Joint width; 0 to 40 ft. member length $\pm 1/2$ in. 41 to 60 ft. member length $\pm 3/4$ in. Differential top elevation as erected. $3/4$ in. Covered with topping $3/4$ in. Untopped floor $1/4$ in. Untopped floor $\frac{1}{4}$ in. Differential top elevation as erected. $3/4$ in. Bearing length ³ (span direction) $\pm 3/4$ in.
e f g		Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum
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e f g		Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum. ±1 in. Plan location from centerline of steel ¹ ±1 in. Plan location from nonminal elevation at member ends Covered with topping ±3/4 in Untopped floor ±1/4 in. Maximum jog in alighment of matching edge (both topped and untopped construction) ±1 in. Joint width ; 0 to 40 ft. member length ±1/4 in. Differential top elevation as erected. Covered with topping 3/4 in. Untopped floor 1/4 in. Differential top elevation of exposed hollowcore slabs ⁴ 1/4 in.
e f	RE .0(= = = = =	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum. ±1 in. Plan location from centerline of steel ¹ . ±1 in. Top elevation from nonminal elevation at member ends Covered with topping. ± ³ / ₄ in Untopped floor. ± ¹ / ₄ in. Maximum jog in alighment of matching edge (both topped and untopped construction) ±1 in. Joint width ; 0 to 40 ft. member length ± ¹ / ₂ in. 41 to 60 ft. member length ± ¹ / ₂ in. 61 ft. plus ±1 in. Differential top elevation as erected. Covered with topping <u>3</u> / ₄ in. Untopped floor. ½ ⁴ / ₄ in. Differential top elevation as erected. Covered with topping <u>3</u> / ₄ in. Untopped floor. ½ ⁴ / ₄ in. Differential top elevation as erected. Covered with topping <u>3</u> / ₄ in. Untopped floor. ½ ⁴ / ₄ in. Differential bottom elevation of exposed hollowcore slabs⁴ ¼ ⁴ in.
e f g	= RE .0(Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum
e f g		Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum
e f g	= = = = = = =	Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum. ±1 in. Plan location from centerline of steel ¹ ±1 in. Top elevation from nonminal elevation at member ends Covered with topping ± ³ / ₄ in Untopped floor ± ¹ / ₄ in. Maximum jog in alighment of matching edge (both topped and untopped construction) ±1 in. Joint width ; 0 to 40 ft. member length ± ¹ / ₂ in. 41 to 60 ft. member length ± ¹ / ₄ in. Differential top elevation as erected. Covered with topping 3/ ₄ in. Untopped floor. ½/ ₄ in. Differential bottom elevation of exposed hollowcore slabs ⁴ . ¼ in. Differential bottom elevation of exposed hollowcore slabs ⁴ . ¼ in. Differential bottom elevation of exposed hollowcore slabs ⁴ . ¼ in. Differential bottom elevation of exposed hollowcore slabs ⁴ . ¼ in. Differential bottom elevation of exposed hollowcore slabs ⁴ . ¼ in.
e f g		Applications requiring close control of differential camber between adjacent members of the same design should be discussed in detail with the producer to determine applicable tolerances. CTION TOLERANCES: HOLLOWCORE DR & ROOF MEMBERS Plan location from building grid datum. ±1 in. Plan location from centerline of steel ¹ ±1 in. Top elevation from nonminal elevation at member ends Covered with topping. ± ³ / ₄ in Untopped floor. ±1/ ₄ in. Maximum jog in alighment of matching edge (both topped and untopped construction). ±1 in. Joint width ; 0 to 40 ft. member length. ± ¹ / ₂ in. 41 to 60 ft. member length. ± ¹ / ₄ in. Differential top elevation as erected. Covered with topping. ¼ ⁴ / ₄ in. Differential top elevation of exposed hollowcore slabs ⁴ . 1/ ₄ in. Differential bottom elevation of exposed hollowcore slabs ⁴ . 1/ ₄ in. Differential bottom elevation of exposed hollowcore slabs ⁴ . 1/ ₄ in.



- CROSS SECTION
- ¹ For precast concrete erected on a steel frame building, this tolerance takes precedence over tolerance on dimension "a".

 2 It may be necessary to feather the edges to $\pm^{1/4}$ in. to properly apply some roof membranes.

³ This is a setting tolerance and should not be confused with structural performance requirements set by the architect/engineer.

⁴ Untopped installation will require a larger tolerance here.





Precast element to structural steel

Infrastructure[™] **Oldcastle**

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF

E8" x 48" Section with no topping

	32		72			
	31	63	78			
	30	70	85			
	29	76	91			
	28	83	66			
	27	89	107			
	26	98	117			
	25	106	127			
	24	116	139			-UDED)
EE	23	127	152			DV INCI
NIN	22	139	166			ALREAL
SPA	21	153	183			HT IS /
CLEAF	20	170	202			F WEIG
	19	188	218			NK SEL
	18	209	233			: (PLA
	17	232	250			10 PSF
	16	250	269			UE > 1
	15	271	290			LE VAL
	14	294	316			JR TAB
	13	322	345			OOK FC
	12	354	379) LL, L
	11	393	421			+ 10(
	10	441	471			D 10 D
ØVcw Kip / Ft		2.90	2.90			: IF YOU NEE
Ultimate Bending Moment,	KipFt / Ft	21.95	29.11			FOR EXAMPLE
P/S Strand Area Sq. in		0.765	1.071			
7-Wire 270 Lolax	[5] 1/2"Ø	[7] 1/2"Ø				
Plank Designation	2008805	2008807				

NOTES:

- Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads. Ч.
 - Table values comply with L/360 deflection limits.
- For combined SDL & LL, your effective required loading is (1.2/1.6) ω. 4.
 - For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table. *SDL + LL <u>с</u>.
- Topping thickness will be minimum at L/2 where camber is highest. Camber can be approximated as 0.3% of the span and must be taken into account when specifying concrete topping thickness. . 0
- For special non-uniform loading conditions, consult Oldcastle. ~ ~ ~
- In residential buildings, add 15± psf to your total uniform loading to account for MEP openings in preliminary design.

Area = 207 in.^2 bw = 10.0 in.

f'ci = 3,000 psi lc = 1,580 in.⁴

f'pu = 270, 000 psi

f'c = 5,000 psi

Consult PCI "Manual for Design of Hollowcore Plank" for detailed design methodology and information. 9.



Infrastructure[®] **Oldcastle**

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF

E8" x 48" Section with 2" bonded structural topping

	2		0			
			1 8			
	3		0			
	9	9	9 10			
	17	3 2	0 10			
	7 23	9;	1 12			
	0 2	7 10	4 13			-
	2	8 11	8 14	 _	-	
	4 2	43 12	74 15	-	-	ED)
	3 2	57 12	32 17	-	-	NCLUD
I FEET	2 2	74 15	13	-	-	EADY
SPAN IN	1 2	94 1:	28 2	 -	 -	IS ALR
LEAR 9	0 2	17 19	42 22	-	-	/EIGHT
0	9 2	13 2-	59 24	-	-	SELF W
	8	53 24	77 29	-	 -	LANK
	7 1	33 26	38 27	-	-	PSF (F
	6 1	05 28	22 29	 -	-	> 110
	5	31 31	48 3.	 -	 -	VALUE
	4	61 3;	79 3,		-	TABLE
	3	95 3	15 3	-	-	K FOR
	1	36 3	58 4	-	-	T, L00
	-	85 4	09 4	 -	-	+ 100 [
	10	45 4	72 5	 -	-	10 DL -
		2	2	 -	-	NEED
ØVcw Kip / F		3.83	3.83			E: IF YOU
Ultimate Bending Moment,	KipFt / Ft	28.76	38.35			FOR EXAMPL
P/S Strand Area Sq. in.		0.765	1.071			
7-Wire 270 Lolax P/S Strand		[5] 1/2"Ø	[7] 1/2"Ø			
Plank Designation	2008805T	2008807T				

NOTES:

- Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads. с.
 - Table values comply with L/360 deflection limits. с. С
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL 4
 - For 100 psf corridor loading, 15 psf usually can be distributed to <u>с</u>.
 - Camber can be approximated as 0.3% of the span and must be adjacent planks and check for 85 psf in load table. . 0
- Topping thickness will be minimum at L/2 where camber is highest. taken into account when specifying concrete topping thickness. For special non-uniform loading conditions, consult Oldcastle.
- In residential buildings, add 15± psf to your total uniform loading to
 - Consult PCI "Manual for Design of Hollowcore Plank" for detailed account for MEP openings in preliminary design. design methodology and information. б.

Area = 207 in.^2 bw = 10.0 in.

Plank self weight with 2" topping is 54 + 25 = 79 psf

f'ci = 3,000 psi Ic= 3,072 in.⁴

f'pu = 270, 000 psi

f'c = 5,000 psi



Infrastructure^w **Oldcastle**

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF H8" x 48" Section with no topping

	32		74			
	31		83			
	30	99	92			
	29	74	102			
	28	84	113			
	27	94	125			
	26	106	134			
	25	119	146			
	24	134	157			UDED)
E	23	148	171			N INCL
N IN F	22	161	187			ILREAD
I SPAI	21	176	205			HT IS A
CLEAF	20	194	225			F WEIG
U	19	213	249			IK SELI
	18	236	276			(PLAN
	17	263	308			10 PSF
	16	295	345			JE > 1
	15	333	389			E VALI
	14	378	435			r tabi
	13	434	475			OK FO
	12	490	521) LL, LC
	7	543	577			+ 100
	10	607	645			0 10 DI
<u>م</u> بل		6	6			U NEEL
ØVc Kip		3.9	3.9			LE: IF YO
Ultimate Bending Moment, ØMn KipFt / Ft		21.95	29.29			FOR EXAMP
P/S Strand Area Sq. in.		0.765	1.071			
7-Wire 270 Lolax P/S Strand		[5] 1/2"Ø	[7] 1/2"Ø			
P lank Designation		3008805	3008807			

NOTES:

- Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads. с.
 - Table values comply with L/360 deflection limits. с. С
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL 4
 - For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table. <u>с</u>.
- Topping thickness will be minimum at L/2 where camber is highest. taken into account when specifying concrete topping thickness. Camber can be approximated as 0.3% of the span and must be . 0
- For special non-uniform loading conditions, consult Oldcastle. In residential buildings, add $15\pm$ psf to your total uniform loading to $\sim \infty$
 - account for MEP openings in preliminary design.
 - Consult PCI "Manual for Design of Hollowcore Plank" for detailed design methodology and information. б.



Plank self weight is 60 psf f'ci = 3,000 psi lc = 1,667 in.⁴ f'c = 5,000 psi

Area = 230 in.² bw = 13.77 in.

f'pu = 270, 000 psi

Oldcastle Infrastructure

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF H8" x 48" Section with 2" bonded structural topping

	32		74			
	31		86			
	30	59	66			
	29	71	114			
	28	85	130			
	27	101	148			
	26	118	168			
	25	137	183			_
	24	158	201			-UDED
EET	23	182	219			DY INCI
NIN	22	205	241			ALREAD
SPA	21	225	266			HT IS /
CLEAF	20	249	294			= WEIG
0	19	276	327			IK SELI
	18	308	365			(PLAN
	17	346	409			10 PSF
	16	390	452			JE > 1
	15	443	489			E VALI
	14	506	531			R TABL
	13	555	580			IOK FO
	12	610	638			LL, LC
	÷	677	707			+ 100
	10	759	792			10 DL
ØVcw Kip / Ft		5.27	5.27			E YOU NEEL
Ultimate Bending Moment,	KipFt / Ft	28.76	38.35			FOR EXAMPLE
P/S Strand Area	Sq. in.	0.765	1.071			
7-Wire 270 Lolax	DIBUG C/A	[5] 1/2 " Ø	[7] 1/2"Ø			
Plank Designation		3008805T	3008807T			

NOTES:

- 1. Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads.
 - Table values comply with L/360 deflection limits.
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL
 - 5. For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table.
 - Camber can be approximated as 0.3% of the span and must be taken into account when specifying concrete topping thickness.
- Topping thickness will be minimum at L/2 where camber is highest. 7. For special non-uniform loading conditions, consult Oldcastle.
- For special non-uniform loading conditions, consult Oldcastle.
 In residential buildings, add 15± psf to your total uniform loading to account for MEP openings in preliminary design.

Area = 230 in.^2 bw = 13.77 in.

Plank self weight with 2" topping is 60 + 25 = 85 psf

f'ci = 3,000 psi lc = 3,143 in.⁴

f'pu = 270, 000 psi

f'c = 5,000 psi

9. Consult PCI "Manual for Design of Hollowcore Plank" for detailed design methodology and information.



Infrastructure[®] **Oldcastle**

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF

H10" x 48" Section with no topping

	38		76			
	37		83			
	36	67	92			
	35	75	100			
	34	83	110			
	33	92	120			
	32	102	132			
	31	112	144			
	30	124	153			
	29	137	164			UDED)
EEL	28	152	176			Y INCL
NIN	27	167	189			LREAD
SPAI	26	179	204			HT IS A
LEAR	25	193	220			: WEIG
0	24	210	238			IK SELF
	23	227	259			(PLAN
	22	248	282			I0 PSF
	21	270	309			JE > 11
	20	296	339			E VALI
	19	327	373			r tabl
	18	361	413			OK FO
	17	402	460			LL, LC
	16	450	515			+ 100
	15	507	564			10 DL
ØVcw Kip / Ft	-	5.47	5.47			F YOU NEEL
						APLE: I
Ultimate Bending Moment,	KipFt / H	35,13	45.13			FOR EXA
P/S Strand Area Sq. in.		0.918	1.224			
7-Wire 270 Lolax P/S Strand		[6] 1/2"Ø	[8] 1/2"Ø			
Plank Designation		3010806	3010808			

NOTES:

- Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads. N.
 - Table values comply with L/360 deflection limits. с. С
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL 4
 - For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table. <u>ю</u>.
- Topping thickness will be minimum at L/2 where camber is highest. taken into account when specifying concrete topping thickness. Camber can be approximated as 0.3% of the span and must be ю.
 - For special non-uniform loading conditions, consult Oldcastle. ~ ~ ~
- In residential buildings, add 15± psf to your total uniform loading to account for MEP openings in preliminary design.
 - Consult PCI "Manual for Design of Hollowcore Plank" for detailed design methodology and information. б.



Area = 271 in.^2 bw = 14.29 in.

f'ci = 3,000 psi lc = 3,080 in.⁴

f'pu = 270, 000 psi

f'c = 5,000 psi

Plank self weight is 71 psf

Oldcastle Infrastructure

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF H10" x 48" Section with 2" bonded structural topping

	38		72			
	37		82			
	36		93			
	35	67	105			
	34	79	118			
	33	92	132			
	32	106	147			
	31	121	164			
	30	137	183			
	29	154	200			UDED)
E	28	174	214			Y INCL
N F	27	196	233			LREAD
SPAN	26	219	251			HT IS A
ILEAR	25	236	272			WEIGH
0	24	259	297			K SELF
	23	281	324			(PLAN
	22	307	355			0 PSF
	21	338	390			JE > 11
	20	372	429			E VALL
	19	412	472			R TABL
	18	458	506			OK FO
	17	512	545			LL, LO
	16	575	589			+ 100
	15	631	640			10 DL
 _ z tī			_) NEED
ØVc Kip /		6.8(6.8(-E: IF YOI
Ultimate Bending Moment, ØMn KipFt / Ft		45.05	55.32			FOR EXAMPI
P/S Strand Area Sq. in.		0.918	1.224			
7-Wire 270 Lolax P/S Strand		[6] 1/2 0	[8] 1/2 ⁼ Ø			
Plank Designation		3010806T	3010808T			

NOTES:

- 1. Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads.
 - Table values comply with L/360 deflection limits.
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL
- 5. For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table.
 - Camber can be approximated as 0.3% of the span and must be taken into account when specifying concrete topping thickness.
- Topping thickness will be minimum at L/2 where camber is highest. 7. For special non-uniform loading conditions, consult Oldcastle.
- For special non-uniform loading conditions, consult Oldcastle.
 In residential buildings, add 15± psf to your total uniform loading to account for MEP openings in preliminary design.

Area = 271 in.^2 bw = 14.29 in.

Plank self weight with 2" topping is 71 + 25 = 96 psf

f'ci = 3,000 psi Ic= 5,263 in.⁴

f'c = 5,000 psi f'pu = 270, 000 psi

> Consult PCI "Manual for Design of Hollowcore Plank" for detailed design methodology and information.



Oldcastle Infrastructure

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF N12" x 48" Section with no topping

	45				72		
	44			68	78		
	43			215	85		
	42		69	81	92		
	41		76	89	100		
	40		84	97	108		
	39	60	92	105	118		
	38	68	101	114	127		
	37	76	110	124	138		
	36	85	120	135	150		
	35	94	131	147	158		UDED)
E	34	103	143	159	168		I/ INCL
N IN F	33	113	156	170	179		LREAD
I SPAI	32	124	170	180	190		HT IS A
CLEAF	31	136	181	193	203		= WEIG
0	30	150	194	205	216		IK SELI
	29	164	207	220	232		(PLAN
	28	181	222	235	248		10 PSF
	27	199	238	253	267		UE > 1
	26	219	257	272	287		-E VAL
	25	240	276	293	310		r tabi
	24	258	298	317	335		JOK FO
	23	281	324	344	364) LL, L(
	22	304	352	375	396		- + 100
	21	332	385	409	432		0 10 DI
	20	364	422	449	474		U NEEL
ØVcw Kip / Ft		6.78	6.78	6.78	6.78		MPLE: IF YO
timate ending oment, 0Mn oFt / Ft		37.74	51.25	57.73	53.93		FOR EXA
P/S Strand Area Sq. in.		0.765	1.071	1.224	1.377		
7-Wire 270 Lolax P/S Strand		[5] 1/2"Ø	[7] 1/2"Ø	[8] 1/2"Ø	[9] 1/2"Ø		
Plank Designation		2012805	2012807	2012808	2012809		

NOTES:

- 1. Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads.
 - Table values comply with L/360 deflection limits.
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL
 - 5. For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table.
- Camber can be approximated as 0.3% of the span and must be taken into account when specifying concrete topping thickness. Topping thickness will be minimum at L/2 where camber is highest.
 - For special non-uniform loading conditions, consult Oldcastle.
 In residential buildings, add 15± psf to your total uniform loading
- 8. In residential buildings, add 15± psf to your total uniform loading to account for MEP openings in preliminary design.

Area = 307 in.²

bw = 14.25 in.

f'ci = 3,000 psi lc = 5,246 in.⁴

f'pu = 270, 000 psi

f'c = 5,000 psi

 Consult PCI "Manual for Design of Hollowcore Plank" for detailed design methodology and information.



Infrastructure[™] A GRH COMPANY **Oldcastle**

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF N12" x 48" Section with 2" bonded structural topping

	45				62		
	44				71		
	43			64	81		
	42			74	60		
	41		99	84	100		
	40		76	95	11		
	39		87	106	123		
	38		66	118	135		
	37	99	111	131	149		
	36	11	125	145	164		
	35	89	139	160	180		(DED)
EI	34	103	155	177	195		IV INCL
NIN	33	117	172	195	208		ILREAD
SPAI	32	134	190	210	223		HT IS A
CLEAF	31	151	210	226	239		= WEIG
0	30	169	225	241	256		IK SELF
	29	186	243	260	275		(PLAN
	28	205	261	279	295		10 PSF
	27	227	282	301	318		JE > 1
	26	251	304	325	344		E VALI
	25	278	330	352	373		R TABL
	24	307	358	382	405		OK FO
	23	333	390	417	441) LL, L(
	22	365	426	455	482		+ 100
	21	399	467	499	513		10 DL
	20	439	514	547	547		U NEED
ØVcw Kip / Ft	ØVcw GP / Ft		8.10	8.10	8.10		APLE: IF YO
Ultimate Bending Moment, ØMn KipFt / Ft		44.56	60.19	67.78	75.20		FOR EXA
P/S Strand Area Sq. in.		0.765	1.071	1.224	1.377		
7-Wire 270 Lolax P/S Strand		[5] 1/2"Ø	[7] 1/2"Ø	[8] 1/2"Ø	[9] 1/2"Ø		
Plank Designation		2012805T	2012807T	2012808T	2012809T		

NOTES:

- Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads. с.
 - Table values comply with L/360 deflection limits. с. С
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL 4
- For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table. <u>л</u>.
 - taken into account when specifying concrete topping thickness. Camber can be approximated as 0.3% of the span and must be . O
- Topping thickness will be minimum at L/2 where camber is highest. For special non-uniform loading conditions, consult Oldcastle. .. ∞
 - n residential buildings, add 15± psf to your total uniform loading to

Area = 307 in.^2

bw = 14.25 in.

f'ci = 3,000 psi lc = 8,393 in.⁴

f'pu = 270, 000 psi

f'c = 5,000 psi

Consult PCI "Manual for Design of Hollowcore Plank" for detailed account for MEP openings in preliminary design. design methodology and information. . О



Infrastructure^w **Oldcastle**

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF

E16" x 48" Section with no topping

	55			78		
	54		63	84		
	53		69	60		
	52		75	96		
	51		82	101		
	50	61	89	106		
	49	68	96	112		
	48	74	103	118		
	47	82	111	124		
	46	90	117	130		
	45	86	123	137		UDED)
EET	44	107	129	145		IN INCL
N IN F	43	116	137	152		ILREAD
SPA	42	126	145	161		HT IS /
CLEAR	41	134	152	170		= WEIG
0	40	141	161	179		IK SELF
	39	150	171	190		(PLAN
	38	158	181	201		10 PSF
	37	168	191	213		UE > 1
	36	179	203	225		LE VAL
	35	189	216	239		IR TAB
	34	202	229	254		DOK FC
	33	215	244	270) LL, L
	32	229	260	288		L + 10(
	31	245	278	307		D 10 D
	30	262	297	328		U NEEI
ØVcw Kip / Ft		7.47	7.47	7.47		AMPLE: IF YC
Ultimate Bending Moment, ØMn KipFt / Ft		73.43	92.15	109.77		FOR EX
P/S Strand Area Sq. in.		1.071	1.377	1.683		
7-Wire 270 Lolax P/S Strand		[7] 1/2"0	[9] 1/2∎Ø	[11] 1/2"Ø		
Plank Designation		2016807	2016809	2016811		

NOTES:

- Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads. с.
 - Table values comply with L/360 deflection limits. с. С
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL 4
 - For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table. <u>с</u>.
- Topping thickness will be minimum at L/2 where camber is highest. taken into account when specifying concrete topping thickness. Camber can be approximated as 0.3% of the span and must be . 0
- For special non-uniform loading conditions, consult Oldcastle. In residential buildings, add $15\pm$ psf to your total uniform loading to $\sim \infty$
 - account for MEP openings in preliminary design.
 - Consult PCI "Manual for Design of Hollowcore Plank" for detailed design methodology and information. б.

bw = 11.3 in.

f'pu = 270, 000 psi



Oldcastle Infrastructure A COMPANY

ELEMATIC[®] HOLLOWCORE PLANK

UNIFORMLY DISTRIBUTED LIVE LOAD CAPACITY IN PSF E16" x 48" Section with 2" bonded structural topping

46 47 48 49 50 51 52 53 54 55 78 69 60 7 7 7 7 7 118 107 97 73 69 61 7 7 7 118 107 97 78 69 61 7 7 7 113 101 125 117 108 99 91 83 75 67 113 131 125 117 108 99 91 83 75 67	
46 47 48 49 50 51 53 54 78 69 60 78 78 69 78 78 79 74 1118 107 97 87 78 69 60 78 73 75 1118 107 97 87 78 69 61 78 75 112 113 125 117 108 99 91 83 75 113 125 117 108 99 91 83 75	
46 47 48 49 50 51 52 53 78 69 60 72 89 50 51 52 53 118 107 97 87 78 69 61 71 113 107 97 87 78 69 61 71 113 131 125 117 108 99 91 83 113 131 125 137 126 13 93	
46 47 48 49 50 51 52 78 69 60 78 78 61 78 118 107 97 87 78 60 61 118 107 97 87 78 69 61 113 101 125 117 108 99 91 113 125 117 108 99 91	
46 47 48 49 50 51 78 69 60 77 69 60 118 107 97 87 78 69 118 107 97 87 78 69 118 107 97 78 69 60 119 107 97 78 69 60 110 107 97 78 69 60 111 107 97 78 69 60 111 105 117 108 99 99 111 105 117 108 99 99	
46 47 48 49 50 46 47 48 49 50 78 69 60 78 78 1118 107 97 87 78 1139 131 125 117 108 1139 131 125 117 108	
46 47 48 49 78 69 60 71 1118 107 97 87 113 107 97 87 113 107 97 87 113 107 97 87 113 107 97 87 114 107 97 87 113 107 97 87 113 107 97 87 114 107 97 87	
46 47 48 46 47 48 78 69 60 1118 107 97 1139 131 125	
46 47 46 47 78 69 118 107 139 131	
46 78 118 139	
45 88 128 148	UDED)
FET 44 44 99 99 1138 156	DV INCL
43 111 147 166	ALREAD
SPA 123 156 176	HT IS /
CLEAF 41 165 186	F WEIG
40 150 150 198	NK SEL
39 162 210	: (PLA)
38 172 223	10 PSF
37 183 212 237	UE > 1
36 196 225 252	LE VAL
35 209 269	JR TAB
34 224 257 287	DOK FC
33 239 274 306	0 LL, L
32 256 294 327	L + 10
31 275 315 350	D 10 D
30 295 337 375	U NEE
00000000000000000000000000000000000000	I MPLE: IF YC
Ultimate Bending Moment, MMn KipFt / Fr 103.34 103.34 123.72	FOR EX
P/S P/S Strand Area Sq. in. 1.071 1.377 1.683	-
7-Wire 270 Lolax P/S Strand [7] 1/2"0 [9] 1/2"0 [11] 1/2"0	
Plank Designation 2016807T 20168011T 2016811T	_

NOTES:

- 1. Design Standard: ACI 318-2014
- Plank self weight and concrete composite topping are both included and do not need to be added to your design loads.
 - Table values comply with L/360 deflection limits.
- For combined SDL & LL, your effective required loading is (1.2/1.6) *SDL + LL
 - 5. For 100 psf corridor loading, 15 psf usually can be distributed to adjacent planks and check for 85 psf in load table.
 - 6. Camber can be approximated as 0.3% of the span and must be taken into account when snacifiving concrete tonning thickness
- To popping thickness will be minimum at L/2 where camber is highest.
- For special non-uniform loading conditions, consult Oldcastle.
 In residential buildings, add 15± psf to your total uniform loading to
 - account for MEP openings in preliminary design. 9. Consult PCI "Manual for Design of Hollowcore Plank" for detailed

Area = 365 in.²

f'ci = 3,000 psi lc= 16,348 in.⁴

f'pu = 270, 000 psi

f'c = 5,000 psi

bw = 11.3 in.

Consult PCI "Manual for Design of Hollowcore Plank" for detaile design methodology and information.

























































MARKET SEGMENTS

Oldcastle Infrastructure, Inc. product offering has grown tremendously since the company was founded more than 50 years ago. Now you'll find precast homes that look no different than brick buildings from the turnof-the-century. There are smart classrooms that make learning much easier, thanks to the quiet acoustics, pest and chemical resistance of precast concrete. And in every market segment we serve, new ideas are becoming a reality all the time.

RESIDENTIAL APPLICATION (SINGLE & MULTI-FAMILY)

Apartments
Assisted Living
College Dormitories
Condominiums
Military Barracks/Quarters
Mixed Use
Nursing Homes

HOSPITALITY

| Hotels/Motel(s)

EDUCATIONS

| Academic Institutions

| Classroom Buildings

INDUSTRIAL

| Warehouse / Distribution Centers

LUNCH & LEARN EVENTS

We developed our Lunch and Learn seminars to create an opportunity for architects, engineers and students to learn more about precast concrete principles and usage, earn accredited AIA/CES learning units and enjoy a complimentary lunch along with a plant tour.

COMMITTED TO THE ENVIRONMENT

The products that we manufacture are inherently durable and we're committed to focusing on innovations that make them even more so. In addition to creating products that last, we challenge ourselves to develop innovative strategies for improving environmental performance. We're particularly proud to be involved with numerous LEED-certified projects and look forward to many more to come.

With strategic manufacturing location we cover the Northeast and Mid-Atlantic regions and support a wide variety of groups in our community. In addition to financial contributions, we volunteer our time building homes for those in need through Habitat for Humanity and by giving the students of West Point Engineering Program the opportunity to have their bridge designs manufactured for a national competition.

WE PROUDLY SUPPORT

- | American Cancer Society®
- | Boys and Girls Club of America
- | Civil Air Patrol
- Emergency Medical
- | Technician Volunteers
- | Habitat for Humanity®
- | Regional Food Bank
- | Special Olympics
- | West Point Engineering Program



OLDCASTLE INFRASTRUCTURE

A division of CRH, Oldcastle Infrastructure Inc. is the leading manufacturer of precast concrete and composites in the U.S. With more than 5,000 employees at over 80 locations nationwide, our work has won awards for safety, quality and customer service.

ORDERING INFORMATION

For specific product information please visit oldcastleinfrastructure.com/products/building-structures or call (518) 767-2116 to reach our team of experts.

MANUFACTURING LOCATIONS

| Selkirk, NY Serving the Northeast to Mid-Atlantic regions.

CONTACT INFORMATION

Main office Oldcastle Infrastructure 123 CR 101 Selkirk, NY 12158 Phone: (518) 767-2116 Fax: (518) 767-9390



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